



Inprentus, Inc.  
51 E. Kenyon Road  
Champaign, IL 61820  
217.239.9862  
www.inprentus.com

## 1 Introduction

Inprentus manufactures master diffraction gratings using *mechanical ruling*. A metal film is deposited on a substrate, and gratings are inscribed in this film, one groove at a time, using a diamond tool. Laser interferometers monitor the tool to ensure that each groove is positioned correctly. At a pitch of 400 nm, for example, diffracted-wavefront error is less than  $\lambda/20$ .

Due to the serial writing process, there is no intrinsic constraint on grating size or shape. Multiple-grating masters are supported.

The principal advantage of the mechanical ruling process is the ability to *blaze* gratings for high efficiency. Blazed gratings require particular, low-symmetry groove shapes in order to concentrate diffracted light into a single radiation mode. Since each groove in the metal film is shaped directly by the diamond tool, mechanical ruling is ideal for the production of blazed gratings.

## 2 Master specification worksheet

Choose a substrate. A layer of Au will be deposited on the substrate, and grating(s) will be inscribed into that layer.

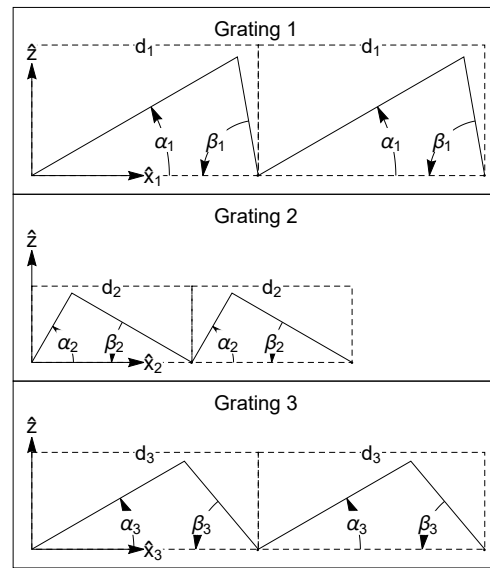
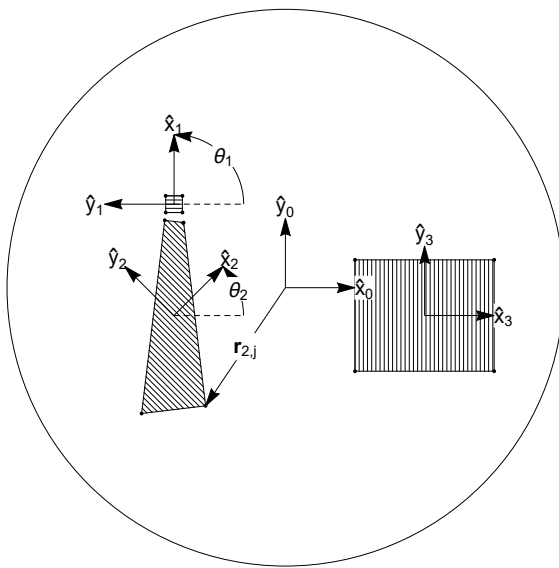
### Substrate description

- SiO<sub>2</sub> circular mirror blank (1-inch diameter, 6-mm thickness)
- SiO<sub>2</sub> circular mirror blank (2-inch diameter, 12-mm thickness)
- SiO<sub>2</sub> square photomask (6-inch edge, 0.25-inch thickness)
- Si circular wafer (4-inch diameter)
- Si circular wafer (6-inch diameter)
- Other (contact Inprentus for details)

Choose a coating. After inscribing grating(s) into the Au film, a conformal capping layer will be desposited.

### Coating description

- None
- Ta (20-nm thickness, oxidized surface is compatible with standard release chemistry)
- Other (contact Inprentus for details)



Symbol	Meaning
$\hat{z}$	Substrate normal
$\hat{x}_0, \hat{y}_0$	Substrate-surface basis
$\hat{x}_i$	Dispersive direction of $i$ th grating
$\hat{y}_i$	Non-dispersive direction of $i$ th grating
$d_i$	Period of $i$ th grating
$\alpha_i$	First groove-facet angle, relative to substrate surface, of $i$ th grating
$\beta_i$	Second groove-facet angle, relative to substrate surface, of $i$ th grating
$\theta_i$	Angle between $\hat{x}_i$ and $\hat{x}_0$
$\mathbf{r}_{i,j}$	For the $i$ th grating, location of $j$ th vertex, relative to substrate origin

Figure 1: Geometric parameters employed in the specification worksheet. The example gratings shown here are for illustration.

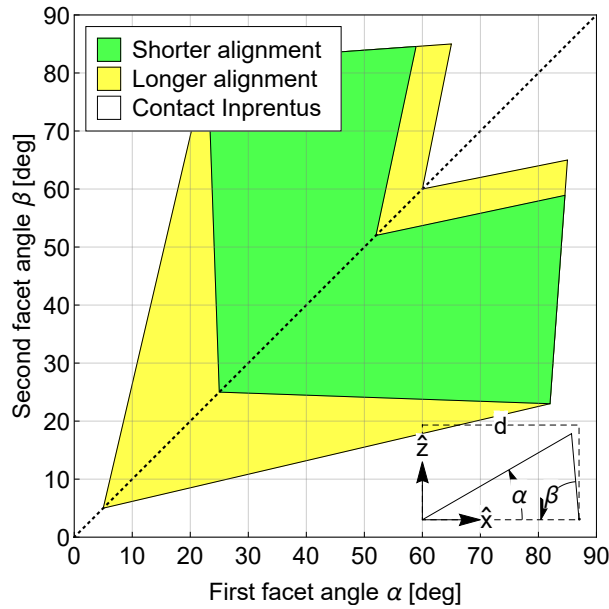


Figure 2: Qualitative difficulty of manufacturing a triangular groove profile with facet angles  $\alpha$  and  $\beta$ . Manufacturing time and cost can be reduced by selecting triangular profiles from the green parameter space.

Define the shape of grating 1 in the substrate-surface plane (see Fig. 1). Express vertices in the substrate coordinate system; for example,  $x_{1,1} = \mathbf{r}_{1,1} \cdot \hat{\mathbf{x}}_0$ . Non-quadrilateral shapes are supported; contact Inprentus for specification requirements.

Parameter	Value
Rotation [deg]	$\theta_1 =$
Vertex 1 [mm]	$x_{1,1} =$ <span style="float: right;"><math>y_{1,1} =</math></span>
Vertex 2 [mm]	$x_{1,2} =$ <span style="float: right;"><math>y_{1,2} =</math></span>
Vertex 3 [mm]	$x_{1,3} =$ <span style="float: right;"><math>y_{1,3} =</math></span>
Vertex 4 [mm]	$x_{1,4} =$ <span style="float: right;"><math>y_{1,4} =</math></span>

Define the shape of the grooves in grating 1 (see Fig. 1). Configuring a diamond tool to produce a particular groove shape is a non-recurring, but potentially protracted, process. Manufacturing time and cost can be reduced by selecting a triangular profile from the green parameter space shown in Fig. 2.

Parameter	Value
Period [nm]	$d_1 =$
First facet angle [deg]	$\alpha_1 =$
Second facet angle [deg]	$\beta_1 =$



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Additional gratings on this substrate can be defined below. If multiple *independent* gratings are desired—for example, iterations on a single grating design—manufacturing time and cost can be reduced by placing each grating on a separate substrate to parallelize the writing process.

Minimum separation between gratings is 1  $\mu\text{m}$ . Uncertainty in grating rotation,  $\theta$ , is 10  $\mu\text{rad}$  or 2 arcsec.

Define the shape of grating 2 in the substrate-surface plane (see Fig. 1).

Parameter	Value
Rotation [deg]	$\theta_2 =$
Vertex 1 [mm]	$x_{2,1} =$ <span style="float: right;"><math>y_{2,1} =</math></span>
Vertex 2 [mm]	$x_{2,2} =$ <span style="float: right;"><math>y_{2,2} =</math></span>
Vertex 3 [mm]	$x_{2,3} =$ <span style="float: right;"><math>y_{2,3} =</math></span>
Vertex 4 [mm]	$x_{2,4} =$ <span style="float: right;"><math>y_{2,4} =</math></span>

Define the shape of the grooves in grating 2 (see Fig. 1).

Parameter	Value
Period [nm]	$d_2 =$
First facet angle [deg]	$\alpha_2 =$
Second facet angle [deg]	$\beta_2 =$

Define the shape of grating 3 in the substrate-surface plane (see Fig. 1).

Parameter	Value
Rotation [deg]	$\theta_3 =$
Vertex 1 [mm]	$x_{3,1} =$ <span style="float: right;"><math>y_{3,1} =</math></span>
Vertex 2 [mm]	$x_{3,2} =$ <span style="float: right;"><math>y_{3,2} =</math></span>
Vertex 3 [mm]	$x_{3,3} =$ <span style="float: right;"><math>y_{3,3} =</math></span>
Vertex 4 [mm]	$x_{3,4} =$ <span style="float: right;"><math>y_{3,4} =</math></span>

Define the shape of the grooves in grating 3 (see Fig. 1).

Parameter	Value
Period [nm]	$d_3 =$
First facet angle [deg]	$\alpha_3 =$
Second facet angle [deg]	$\beta_3 =$